



## **Factual Power Loss Reduction by Augmented Monkey Optimization Algorithm**

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### **A B S T R A C T**

This paper presents Augmented Monkey Optimization Algorithm (AMOA) applied to solve optimal reactive power problem. Communal behaviour of monkeys has been utilized to model the algorithm. Normally, group monkeys assess the distance from the source to food for foraging behaviour. Local leader renews its most excellent location inside the group, when the food source is not rationalized then the group will start probing in different directions for the food sources. Two most important control parameters are Global Leader Limit (GLlimit) and Local Leader Limit (LLlimit) which give appropriate way to global and local leaders correspondingly. Levy flight has been intermingled in the algorithm to enhance the search ability. Proposed AMOA accelerates the exploitation ability that has been tested in standard IEEE 14, 30, 57, 118, 300 bus test systems. The simulation results show the projected algorithm reduced the real power loss comprehensively.

**Keywords:** Optimal reactive power, Transmission loss, Augmented monkey optimization algorithm.

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## **1. Introduction**

Reactive power problem plays a key role in secure and economic operations of power system. Optimal reactive power problem has been solved by variety of types of methods [1-6]. Nevertheless, numerous scientific difficulties are found while solving problem due to an assortment of constraints. Evolutionary techniques [7-16] are applied to solve the reactive power problem, but the main problem is the many algorithms get stuck in local optimal solution and fail to balance the exploration and exploitation during the search of global solution. In this paper, AMOA has been applied to solve the optimal reactive power problem. Communal behavior of monkeys has been utilized to model the algorithm. Normally, group monkeys assess the distance from the source to food for foraging behavior. Based on the distance from the foods source, the

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group members will modernize their location and estimation will be done again from the food to the source. Local leader renews its most excellent location inside the group, when the food source is not rationalized, then the group will start probing in different directions for the food sources. Two most important control parameters are GLimit and LLimit which give appropriate way to global and local leaders correspondingly. Levy flight has been intermingled in the algorithm to enhance the search ability. Proposed AMOA accelerates the exploitation ability. Proposed algorithm has been tested in standard IEEE 14, 30, 57,118,300 bus test system and simulation results show the projected algorithm reduced the real power loss extensively.

## 2. Problem Formulation

Objective of the problem is to reduce the true power loss:

$$F = P_L = \sum_{k \in Nbr} g_k (V_i^2 + V_j^2 - 2V_i V_j \cos \theta_{ij}). \tag{1}$$

Voltage deviation given as follows:

$$F = P_L + \omega_v \times \text{Voltage Deviation}. \tag{2}$$

Voltage deviation given by:

$$\text{Voltage Deviation} = \sum_{i=1}^{Npq} |V_i - 1|, \tag{3}$$

Constraint (equality):

$$P_G = P_D + P_L, \tag{4}$$

Constraints (inequality):

$$P_{gslack}^{\min} \leq P_{gslack} \leq P_{gslack}^{\max}, \tag{5}$$

$$Q_{gi}^{\min} \leq Q_{gi} \leq Q_{gi}^{\max}, i \in N_g, \tag{6}$$

$$V_i^{\min} \leq V_i \leq V_i^{\max}, i \in N, \tag{7}$$

$$T_i^{\min} \leq T_i \leq T_i^{\max}, i \in N_T, \tag{8}$$

$$Q_c^{\min} \leq Q_c \leq Q_c^{\max}, i \in N_C. \tag{9}$$

## 3. Augmented Monkey Optimization Algorithm

Communal behavior of monkeys has been utilized to model the algorithm. Normally, group monkeys assess the distance from the source to food for foraging behavior. Based on the distance from the foods source, the group members will modernize their location and estimation will be done again from the food to the source. Local leader renews its most excellent location inside the group, when the food source is not rationalized then the group will start probing in different

directions for the food sources [17]. Two most important control parameters are GLlimit and LLlimit which give appropriate way to global and local leaders correspondingly.

**Population Initialization.** Primary population of “N” monkeys where each monkey  $SM_i$  ( $i = 1, 2, \dots, N$ ) is a vector of dimension D. Every monkey ( $SM_i$ ) is initialized by:

$$SM_{ij} = SM_{\min j} + \emptyset \times (SM_{\max j} - SM_{\min j}). \quad (10)$$

**Local Leader Phase (LLP).** For new-fangled location, the fitness value will be computed. Updating of locations will be done based on the fitness value.

$$SM_{\text{newij}} = SM_{ij} + \emptyset_1 \times (LL_{kj} - SM_{ij}) + \emptyset_2 \times (SM_{rj} - SM_{ij}), \quad (11)$$

where  $\emptyset_1 \in (0,1)$  and  $\emptyset_2 \in (-1,1)$ .

**Global Leader Phase (GLP).** In this phase all the SMs modernize their location by Global Leader and local group member's indulgent and done by:

$$SM_{\text{newij}} = SM_{ij} + \emptyset_1 \times (GL_j - SM_{ij}) + \emptyset_2 \times (SM_{rj} - SM_{ij}), \quad (12)$$

where  $\emptyset_1 \in (0,1)$  and  $\emptyset_2 \in (-1,1)$ .

In GLP phase, monkey's ( $SM_i$ ) locations are rationalized based on probability  $p_i$  and computed by:

$$p_i = 0.90 \times \frac{\text{fitness}_i}{\text{fitness}_{\text{maximum}}} + 0.10. \quad (13)$$

**Global Leader Learning (GLL) Phase.** Global leader location is rationalized by applying the voracious selection procedure in the population, the stupendous fitness in the population is chosen as the rationalized location of the global leader. Additionally, when global leader is not updated then global limit count is incremented by 1.

**Local Leader Learning (LLL) Phase.** Local leader position is rationalized by employing the greedy selection, the rationalized location of the local leader is evaluated by comparing with the older one; when the local leader is not rationalized then the local limit count is incremented by 1.

**Local Leader Decision (LLD) Phase.** All members of group renew their locations by capricious initialization when the local leader position is not modernized,

$$SM_{\text{newij}} = SM_{ij} + \emptyset \times (GL_j - SM_{ij}) + \emptyset \times (SM_{ij} - LL_{kj}), \quad (14)$$

where  $\emptyset \in (0,1)$ .

**Global Leader Decision (GLD) Phase.** Global leader split the population into smaller groups when the position of global leader is not modernized and at first population is alienated into two groups, then three groups and so on until maximum number of groups are formed. Every time in GLD segment, LLL process is instigate to make a decision on the local leader in the newly formed groups.

Levy flight is a rank of non-Gaussian random procedure whose capricious walks are haggard from levy stable distribution. Allocation by  $L(s) \sim |s|^{-1-\beta}$  where  $0 < \beta < 2$  is an index, scientifically defined as:

$$L(s, \gamma, \mu) = \begin{cases} \sqrt{\frac{\gamma}{2\pi}} \exp\left[-\frac{\gamma}{2(s-\mu)}\right] \frac{1}{(s-\mu)^{3/2}} & \text{if } 0 < \mu < s < \infty. \\ 0 & \text{if } s \leq 0 \end{cases} \quad (15)$$

In terms of Fourier transform, the levy distribution defined as:

$$F(k) = \exp[-\alpha|k|^\beta], 0 < \beta \leq 2, \quad (16)$$

fresh state is calculated as:

$$X^{t+1} = X^t + \alpha \oplus \text{Levy}(\beta), \quad (17)$$

$$X^{t+1} = X^t + \text{random}(\text{size}(D)) \oplus \text{Levy}(\beta), \quad (18)$$

non-trivial scheme of engendering step size is defined by:

$$X^{t+1} = X^t + \text{random}(\text{size}(D)) \oplus \text{Levy}(\beta) \sim 0.01 \frac{u}{|v|^{1/\beta}} (x_j^t - gb), \quad (19)$$

$$u \sim N(0, \sigma_u^2) \quad v \sim N(0, \sigma_v^2), \quad (20)$$

with

$$\sigma_u = \left\{ \frac{\Gamma(1+\beta)\sin(\pi\beta/2)}{\Gamma[(1+\beta)/2]\beta 2^{(\beta-1)/2}} \right\}^{1/\beta}, \sigma_v = 1. \quad (21)$$

Here  $\Gamma$  is standard Gamma function. One of the important points to be considered while performing distribution by levy flights is the value taken by the  $\beta$  parameter and it substantially affects distribution.

To accelerate the exploitation ability of the monkey algorithm, a Levy Flight Based Local Search (LFLS) scheme is integrated with it.

In LFLS scheme step size is computed as:

$$\text{Step\_size} = 0.002 \times s(t) \times (x_{\text{best}j} - x_{kj}) \times U(0,1), \quad (22)$$

position renewal of the most excellent individual inside the present population is found by:

$$x'_{bestj}(t+1) = x_{bestj}(t) + Step\_size(t). \quad (23)$$

Key in the optimization function Min  $f(x)$  and  $\beta$ ;  
 Choose the most excellent solution  $x_{best}$ ,  
 Initialize  $t = 1, \sigma_v = 1$ ,  
 Compute  $\sigma_u = \left\{ \frac{\Gamma(1+\beta)\sin(\pi\beta/2)}{\Gamma[(1+\beta)/2]\beta 2^{(\beta-1)/2}} \right\}^{1/\beta}$ ,  
 While ( $t < \epsilon$ ) do,  
 Calculate the step size by;  $Step_{size} = 0.002 \times s(t) \times (x_{bestj} - x_{kj}) \times U(0,1)$ ,  
 Engender a new-fangled solution  $x'_{best}$ ,  
 Compute  $f(x'_{best})$ ; when  $f(x'_{best}) = f(x_{best})$  then  $x_{best} = x'_{best}$ ,  
 End if,  
 $t = t + 1$ ;  
 End while.

Levy flight has been intermingled in the algorithm to enhance the search ability. Proposed AMOA accelerates the exploitation ability.

Parameters values are initialized;  
 While stop criteria do;  
**Step a.** Apply Local Leader phase.  
**Step b.** Apply Global Leader phase.  
**Step c.** Apply Local Leader Learning phase.  
**Step d.** Apply Global Leader Learning phase.  
**Step e.** Apply Local Leader Decision phase.  
**Step f.** Apply Global Leader Decision phase.  
**Step g.** Apply Levy Flight based Local Search Strategy  
 End while.  
 Print the most excellent solution.

## 4. Simulation Results

At first, in standard IEEE 14 bus system, the validity of the proposed AMOA has been tested, **Table 1** shows the constraints of control variables **Table 2** shows the limits of reactive power generators and comparison results are presented in **Table 3**.

**Table 1.** Constraints of control variables.

| System | Variables         | Minimum (PU) | Maximum (PU) |
|--------|-------------------|--------------|--------------|
|        | Generator Voltage | 0.95         | 1.1          |
|        | Transformer Tap   | 0.9          | 1.1          |
|        | VAR Source        | 0            | 0.20         |

**Table 2.** Constrains of reactive power generators.

| System | Variables | Q Minimum (PU) | Q Maximum (PU) |
|--------|-----------|----------------|----------------|
|        | 1         | 0              | 10             |
|        | 2         | -40            | 50             |
|        | 3         | 0              | 40             |
|        | 6         | -6             | 24             |
|        | 8         | -6             | 24             |

**Table 3.** Simulation results of IEEE –14 system.

| Control variables      | Base case | MPSO [19] | PSO [19] | EP [19] | SARGA [19] | AMOA   |
|------------------------|-----------|-----------|----------|---------|------------|--------|
| VG-1                   | 1.060     | 1.100     | 1.100    | NR*     | NR*        | 1.010  |
| VG-2                   | 1.045     | 1.085     | 1.086    | 1.029   | 1.060      | 1.031  |
| VG-3                   | 1.010     | 1.055     | 1.056    | 1.016   | 1.036      | 1.022  |
| VG-6                   | 1.070     | 1.069     | 1.067    | 1.097   | 1.099      | 1.030  |
| VG-8                   | 1.090     | 1.074     | 1.060    | 1.053   | 1.078      | 1.014  |
| Tap 8                  | 0.978     | 1.018     | 1.019    | 1.04    | 0.95       | 0.902  |
| Tap 9                  | 0.969     | 0.975     | 0.988    | 0.94    | 0.95       | 0.910  |
| Tap 10                 | 0.932     | 1.024     | 1.008    | 1.03    | 0.96       | 0.950  |
| QC-9                   | 0.19      | 14.64     | 0.185    | 0.18    | 0.06       | 0.161  |
| PG                     | 272.39    | 271.32    | 271.32   | NR*     | NR*        | 272.06 |
| QG (Mvar)              | 82.44     | 75.79     | 76.79    | NR*     | NR*        | 75.02  |
| Reduction in PLoss (%) | 0         | 9.2       | 9.1      | 1.5     | 2.5        | 16.9   |
| Total PLoss (Mw)       | 13.550    | 12.293    | 12.315   | 13.346  | 13.216     | 11.256 |

NR\* - Not reported.

Then the proposed AMOA has been tested in IEEE 30 bus system. **Table 4** shows the constraints of control variables, **Table 5** shows the limits of reactive power generators, and comparison results are presented in **Table 6**.

**Table 4.** Constraints of control variables.

| System | Variables         | Minimum (PU) | Maximum (PU) |
|--------|-------------------|--------------|--------------|
|        | Generator Voltage | 0.95         | 1.1          |
|        | Transformer Tap   | 0.9          | 1.1          |
|        | VAR Source        | 0            | 0.20         |

**Table 5.** Constrains of reactive power generators.

| System | Variables | Q Minimum (PU) | Q Maximum (PU) |
|--------|-----------|----------------|----------------|
|        | 1         | 0              | 10             |
|        | 2         | -40            | 50             |
|        | 5         | -40            | 40             |
|        | 8         | -10            | 40             |
|        | 11        | -6             | 24             |
|        | 13        | -6             | 24             |

**Table 6.** Simulation results of IEEE –30 system.

| Control variables      | Base case | MPSO [19] | PSO [19] | EP [19] | SARGA [19] | AMOA   |
|------------------------|-----------|-----------|----------|---------|------------|--------|
| VG-1                   | 1.060     | 1.101     | 1.100    | NR*     | NR*        | 1.023  |
| VG-2                   | 1.045     | 1.086     | 1.072    | 1.097   | 1.094      | 1.046  |
| VG-5                   | 1.010     | 1.047     | 1.038    | 1.049   | 1.053      | 1.078  |
| VG-8                   | 1.010     | 1.057     | 1.048    | 1.033   | 1.059      | 1.015  |
| VG-12                  | 1.082     | 1.048     | 1.058    | 1.092   | 1.099      | 1.059  |
| VG-13                  | 1.071     | 1.068     | 1.080    | 1.091   | 1.099      | 1.061  |
| Tap11                  | 0.978     | 0.983     | 0.987    | 1.01    | 0.99       | 0.901  |
| Tap12                  | 0.969     | 1.023     | 1.015    | 1.03    | 1.03       | 0.932  |
| Tap15                  | 0.932     | 1.020     | 1.020    | 1.07    | 0.98       | 0.901  |
| Tap36                  | 0.968     | 0.988     | 1.012    | 0.99    | 0.96       | 0.910  |
| QC10                   | 0.19      | 0.077     | 0.077    | 0.19    | 0.19       | 0.082  |
| QC24                   | 0.043     | 0.119     | 0.128    | 0.04    | 0.04       | 0.139  |
| PG (MW)                | 300.9     | 299.54    | 299.54   | NR*     | NR*        | 299.01 |
| QG (Mvar)              | 133.9     | 130.83    | 130.94   | NR*     | NR*        | 131.06 |
| Reduction in PLoss (%) | 0         | 8.4       | 7.4      | 6.6     | 8.3        | 10.6   |
| Total PLoss (Mw)       | 17.55     | 16.07     | 16.25    | 16.38   | 16.09      | 15.68  |

NR\* - Not reported.

Then the proposed AMOA has been tested in IEEE 57 bus system. **Table 7** shows the constraints of control variables, **Table 8** shows the limits of reactive power generators, and comparison results are presented in **Table 9**.

**Table 7.** Constraints of control variables.

| System | Variables         | Minimum (PU) | Maximum (PU) |
|--------|-------------------|--------------|--------------|
|        | Generator Voltage | 0.95         | 1.1          |
|        | Transformer Tap   | 0.9          | 1.1          |
|        | VAR Source        | 0            | 0.20         |

**Table 8.** Constrains of reactive power generators.

| System | Variables | Q Minimum (PU) | Q Maximum (PU) |
|--------|-----------|----------------|----------------|
|        | 1         | -140           | 200            |
|        | 2         | -17            | 50             |
|        | 3         | -10            | 60             |
|        | 6         | -8             | 25             |
|        | 8         | -140           | 200            |
|        | 9         | -3             | 9              |
|        | 12        | -150           | 155            |

**Table 9.** Simulation results of IEEE –57 system.

| Control variables      | Base case | MPSO [19] | PSO [19] | CGA [19] | AGA [19] | AMOA   |
|------------------------|-----------|-----------|----------|----------|----------|--------|
| VG 1                   | 1.040     | 1.093     | 1.083    | 0.968    | 1.027    | 1.010  |
| VG 2                   | 1.010     | 1.086     | 1.071    | 1.049    | 1.011    | 1.021  |
| VG 3                   | 0.985     | 1.056     | 1.055    | 1.056    | 1.033    | 1.043  |
| VG 6                   | 0.980     | 1.038     | 1.036    | 0.987    | 1.001    | 1.021  |
| VG 8                   | 1.005     | 1.066     | 1.059    | 1.022    | 1.051    | 1.043  |
| VG 9                   | 0.980     | 1.054     | 1.048    | 0.991    | 1.051    | 1.001  |
| VG 12                  | 1.015     | 1.054     | 1.046    | 1.004    | 1.057    | 1.063  |
| Tap 19                 | 0.970     | 0.975     | 0.987    | 0.920    | 1.030    | 0.961` |
| Tap 20                 | 0.978     | 0.982     | 0.983    | 0.920    | 1.020    | 0.940  |
| Tap 31                 | 1.043     | 0.975     | 0.981    | 0.970    | 1.060    | 0.932  |
| Tap 35                 | 1.000     | 1.025     | 1.003    | NR*      | NR*      | 1.010  |
| Tap 36                 | 1.000     | 1.002     | 0.985    | NR*      | NR*      | 1.001  |
| Tap 37                 | 1.043     | 1.007     | 1.009    | 0.900    | 0.990    | 1.000  |
| Tap 41                 | 0.967     | 0.994     | 1.007    | 0.910    | 1.100    | 0.991  |
| Tap 46                 | 0.975     | 1.013     | 1.018    | 1.100    | 0.980    | 1.014  |
| Tap 54                 | 0.955     | 0.988     | 0.986    | 0.940    | 1.010    | 0.982  |
| Tap 58                 | 0.955     | 0.979     | 0.992    | 0.950    | 1.080    | 0.961  |
| Tap 59                 | 0.900     | 0.983     | 0.990    | 1.030    | 0.940    | 0.973  |
| Tap 65                 | 0.930     | 1.015     | 0.997    | 1.090    | 0.950    | 1.012  |
| Tap 66                 | 0.895     | 0.975     | 0.984    | 0.900    | 1.050    | 0.976  |
| Tap 71                 | 0.958     | 1.020     | 0.990    | 0.900    | 0.950    | 1.013  |
| Tap 73                 | 0.958     | 1.001     | 0.988    | 1.000    | 1.010    | 1.001  |
| Tap 76                 | 0.980     | 0.979     | 0.980    | 0.960    | 0.940    | 0.972  |
| Tap 80                 | 0.940     | 1.002     | 1.017    | 1.000    | 1.000    | 1.001  |
| QC 18                  | 0.1       | 0.179     | 0.131    | 0.084    | 0.016    | 0.170  |
| QC 25                  | 0.059     | 0.176     | 0.144    | 0.008    | 0.015    | 0.172  |
| QC 53                  | 0.063     | 0.141     | 0.162    | 0.053    | 0.038    | 0.141  |
| PG (MW)                | 1278.6    | 1274.4    | 1274.8   | 1276     | 1275     | 1261.4 |
| QG (Mvar)              | 321.08    | 272.27    | 276.58   | 309.1    | 304.4    | 270.84 |
| Reduction in PLoss (%) | 0         | 15.4      | 14.1     | 9.2      | 11.6     | 18.5   |
| Total PLoss (Mw)       | 27.8      | 23.51     | 23.86    | 25.24    | 24.56    | 22.642 |

NR\* - Not reported.

Then the proposed AMOA has been tested in IEEE 118 bus system. **Table 10** shows the constraints of control variables and comparison results are presented in **Table 11**.



**Table 10.** Constraints of control variables.

| System | Variables         | Minimum (PU) | Maximum (PU) |
|--------|-------------------|--------------|--------------|
|        | Generator Voltage | 0.95         | 1.1          |
|        | Transformer Tap   | 0.9          | 1.1          |
|        | VAR Source        | 0            | 0.20         |

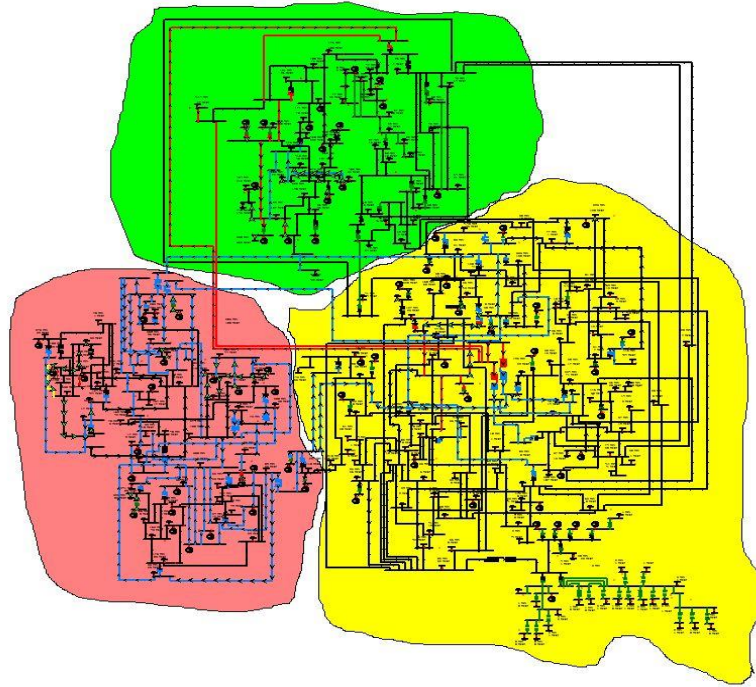
**Table 11.** Simulation results of IEEE –118 system.

| Control variables | Base case | MPSO [19] | PSO [19] | PSO [19] | CLPSO [19] | AMOA  |
|-------------------|-----------|-----------|----------|----------|------------|-------|
| VG 1              | 0.955     | 1.021     | 1.019    | 1.085    | 1.033      | 1.024 |
| VG 4              | 0.998     | 1.044     | 1.038    | 1.042    | 1.055      | 1.040 |
| VG 6              | 0.990     | 1.044     | 1.044    | 1.080    | 0.975      | 1.020 |
| VG 8              | 1.015     | 1.063     | 1.039    | 0.968    | 0.966      | 1.013 |
| VG 10             | 1.050     | 1.084     | 1.040    | 1.075    | 0.981      | 1.027 |
| VG 12             | 0.990     | 1.032     | 1.029    | 1.022    | 1.009      | 1.018 |
| VG 15             | 0.970     | 1.024     | 1.020    | 1.078    | 0.978      | 1.014 |
| VG 18             | 0.973     | 1.042     | 1.016    | 1.049    | 1.079      | 1.039 |
| VG 19             | 0.962     | 1.031     | 1.015    | 1.077    | 1.080      | 1.015 |
| VG 24             | 0.992     | 1.058     | 1.033    | 1.082    | 1.028      | 1.028 |
| VG 25             | 1.050     | 1.064     | 1.059    | 0.956    | 1.030      | 1.048 |
| VG 26             | 1.015     | 1.033     | 1.049    | 1.080    | 0.987      | 1.036 |
| VG 27             | 0.968     | 1.020     | 1.021    | 1.087    | 1.015      | 0.925 |
| VG31              | 0.967     | 1.023     | 1.012    | 0.960    | 0.961      | 0.949 |
| VG 32             | 0.963     | 1.023     | 1.018    | 1.100    | 0.985      | 0.961 |
| VG 34             | 0.984     | 1.034     | 1.023    | 0.961    | 1.015      | 1.024 |
| VG 36             | 0.980     | 1.035     | 1.014    | 1.036    | 1.084      | 1.018 |
| VG 40             | 0.970     | 1.016     | 1.015    | 1.091    | 0.983      | 0.979 |
| VG 42             | 0.985     | 1.019     | 1.015    | 0.970    | 1.051      | 1.019 |
| VG 46             | 1.005     | 1.010     | 1.017    | 1.039    | 0.975      | 1.016 |
| VG 49             | 1.025     | 1.045     | 1.030    | 1.083    | 0.983      | 1.004 |
| VG 54             | 0.955     | 1.029     | 1.020    | 0.976    | 0.963      | 0.954 |
| VG 55             | 0.952     | 1.031     | 1.017    | 1.010    | 0.971      | 0.982 |
| VG56              | 0.954     | 1.029     | 1.018    | 0.953    | 1.025      | 0.969 |
| VG 59             | 0.985     | 1.052     | 1.042    | 0.967    | 1.000      | 0.984 |
| VG 61             | 0.995     | 1.042     | 1.029    | 1.093    | 1.077      | 0.982 |
| VG 62             | 0.998     | 1.029     | 1.029    | 1.097    | 1.048      | 0.990 |
| VG 65             | 1.005     | 1.054     | 1.042    | 1.089    | 0.968      | 1.001 |
| VG 66             | 1.050     | 1.056     | 1.054    | 1.086    | 0.964      | 1.001 |
| VG 69             | 1.035     | 1.072     | 1.058    | 0.966    | 0.957      | 1.051 |
| VG 70             | 0.984     | 1.040     | 1.031    | 1.078    | 0.976      | 1.047 |
| VG 72             | 0.980     | 1.039     | 1.039    | 0.950    | 1.024      | 1.039 |
| VG 73             | 0.991     | 1.028     | 1.015    | 0.972    | 0.965      | 1.020 |
| VG 74             | 0.958     | 1.032     | 1.029    | 0.971    | 1.073      | 1.029 |
| VG 76             | 0.943     | 1.005     | 1.021    | 0.960    | 1.030      | 1.012 |
| VG 77             | 1.006     | 1.038     | 1.026    | 1.078    | 1.027      | 1.032 |
| VG 80             | 1.040     | 1.049     | 1.038    | 1.078    | 0.985      | 1.016 |
| VG 85             | 0.985     | 1.024     | 1.024    | 0.956    | 0.983      | 1.025 |
| VG 87             | 1.015     | 1.019     | 1.022    | 0.964    | 1.088      | 1.019 |
| VG 89             | 1.000     | 1.074     | 1.061    | 0.974    | 0.989      | 1.053 |
| VG 90             | 1.005     | 1.045     | 1.032    | 1.024    | 0.990      | 1.041 |

| Control variables     | Base case | MPSO [19] | PSO [19] | PSO [19] | CLPSO [19] | AMOA   |
|-----------------------|-----------|-----------|----------|----------|------------|--------|
| VG 91                 | 0.980     | 1.052     | 1.033    | 0.961    | 1.028      | 1.038  |
| VG 92                 | 0.990     | 1.058     | 1.038    | 0.956    | 0.976      | 1.029  |
| VG 99                 | 1.010     | 1.023     | 1.037    | 0.954    | 1.088      | 1.008  |
| VG 100                | 1.017     | 1.049     | 1.037    | 0.958    | 0.961      | 1.014  |
| VG 103                | 1.010     | 1.045     | 1.031    | 1.016    | 0.961      | 1.025  |
| VG 104                | 0.971     | 1.035     | 1.031    | 1.099    | 1.012      | 1.014  |
| VG 105                | 0.965     | 1.043     | 1.029    | 0.969    | 1.068      | 1.061  |
| VG 107                | 0.952     | 1.023     | 1.008    | 0.965    | 0.976      | 1.020  |
| VG 110                | 0.973     | 1.032     | 1.028    | 1.087    | 1.041      | 1.016  |
| VG 111                | 0.980     | 1.035     | 1.039    | 1.037    | 0.979      | 1.014  |
| VG 112                | 0.975     | 1.018     | 1.019    | 1.092    | 0.976      | 1.090  |
| VG 113                | 0.993     | 1.043     | 1.027    | 1.075    | 0.972      | 1.028  |
| VG 116                | 1.005     | 1.011     | 1.031    | 0.959    | 1.033      | 1.000  |
| Tap 8                 | 0.985     | 0.999     | 0.994    | 1.011    | 1.004      | 0.949  |
| Tap 32                | 0.960     | 1.017     | 1.013    | 1.090    | 1.060      | 1.003  |
| Tap 36                | 0.960     | 0.994     | 0.997    | 1.003    | 1.000      | 0.951  |
| Tap 51                | 0.935     | 0.998     | 1.000    | 1.000    | 1.000      | 0.942  |
| Tap 93                | 0.960     | 1.000     | 0.997    | 1.008    | 0.992      | 1.000  |
| Tap 95                | 0.985     | 0.995     | 1.020    | 1.032    | 1.007      | 0.989  |
| Tap 102               | 0.935     | 1.024     | 1.004    | 0.944    | 1.061      | 1.014  |
| Tap 107               | 0.935     | 0.989     | 1.008    | 0.906    | 0.930      | 0.965  |
| Tap 127               | 0.935     | 1.010     | 1.009    | 0.967    | 0.957      | 1.002  |
| QC 34                 | 0.140     | 0.049     | 0.048    | 0.093    | 0.117      | 0.014  |
| QC 44                 | 0.100     | 0.026     | 0.026    | 0.093    | 0.098      | 0.010  |
| QC 45                 | 0.100     | 0.196     | 0.197    | 0.086    | 0.094      | 0.172  |
| QC 46                 | 0.100     | 0.117     | 0.118    | 0.089    | 0.026      | 0.114  |
| QC 48                 | 0.150     | 0.056     | 0.056    | 0.118    | 0.028      | 0.031  |
| QC 74                 | 0.120     | 0.120     | 0.120    | 0.046    | 0.005      | 0.128  |
| QC 79                 | 0.200     | 0.139     | 0.140    | 0.105    | 0.148      | 0.119  |
| QC 82                 | 0.200     | 0.180     | 0.180    | 0.164    | 0.194      | 0.165  |
| QC 83                 | 0.100     | 0.166     | 0.166    | 0.096    | 0.069      | 0.148  |
| QC 105                | 0.200     | 0.189     | 0.190    | 0.089    | 0.090      | 0.161  |
| QC 107                | 0.060     | 0.128     | 0.129    | 0.050    | 0.049      | 0.128  |
| QC 110                | 0.060     | 0.014     | 0.014    | 0.055    | 0.022      | 0.014  |
| PG(MW)                | 4374.8    | 4359.3    | 4361.4   | NR*      | NR*        | 4422.5 |
| QG(MVAR)              | 795.6     | 604.3     | 653.5    | * NR*    | NR*        | 627.9  |
| Reduction in PLOSS(%) | 0         | 11.7      | 10.1     | 0.6      | 1.3        | 13.3   |
| Total PLOSS (Mw)      | 132.8     | 117.19    | 119.34   | 131.99   | 130.96     | 115.01 |

NR\* - Not reported.

Then IEEE 300 bus system [18] is used as test system to validate the performance of the AMOA. **Table 12** shows the comparison of real power loss obtained after optimization. **Figure 1** shows IEEE 300 bus system [18] and this IEEE 300-bus system contains 69 generators, 60 LTCs, 304 transmission lines, and 195 loads.



**Figure 1.** IEEE 300-Bus System case [18].

**Table 12.** Comparison of real power loss.

| Parameter  | Method EGA<br>[21] | Method EEA<br>[21] | Method CSA<br>[20] | AMOA     |
|------------|--------------------|--------------------|--------------------|----------|
| PLOSS (MW) | 646.2998           | 650.6027           | 635.8942           | 610.0964 |

## 5. Conclusion

In this work AMOA successfully solved the optimal reactive power problem. Two most important control parameters are GLLimit and LLLimit which give appropriate way to global and local leaders correspondingly. Levy flight has been intermingled in the algorithm to enhance the search ability. Proposed AMOA accelerated the exploitation ability. Proposed has been tested in standard IEEE 14, 30, 57,118,300 bus test systems and simulation results show the projected algorithm reduced the real power loss comprehensively.

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